

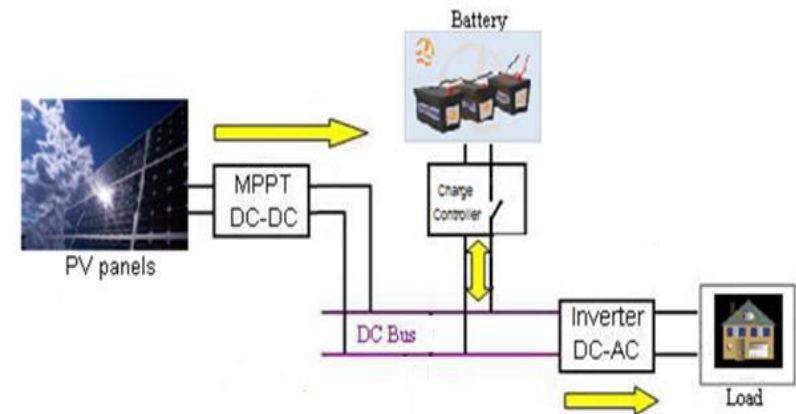
Design and optimization of a standalone photovoltaic system considering panel position, battery lifespan, and cost

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- **INTRODUCTION**
- **STANDALONE PHOTOVOLTAIC SYSTEM**
- **DESIGN OPTIMIZATION PROCEDURE**
- **RESULTS AND DISCUSSIONS**
- **CONCLUSION AND PERSPECTIVES**

- ❖ Solar Home Systems (SHS) have been promoted as an alternative to grid extension especially for isolated sites. These photovoltaic (PV) systems require batteries, minimal costs, and must be reliable.
- ❖ Batteries' size, installation, operation and maintenance are fundamentally different from other energy storage applications.
- ❖ In our previous investigations, we considered both ecological and economic costs for the design optimization of a stand-alone hybrid wind-PV power system that included battery storage. Embodied energy is a relevant objective function where the life cycle of the components is considered.
- ❖ For this new investigation, we propose to thoroughly evaluate lead acid battery lifespan in order to improve the final cost. In this case, batteries replacement dates are not fixed a priori and consequently better optimization results are carried out.

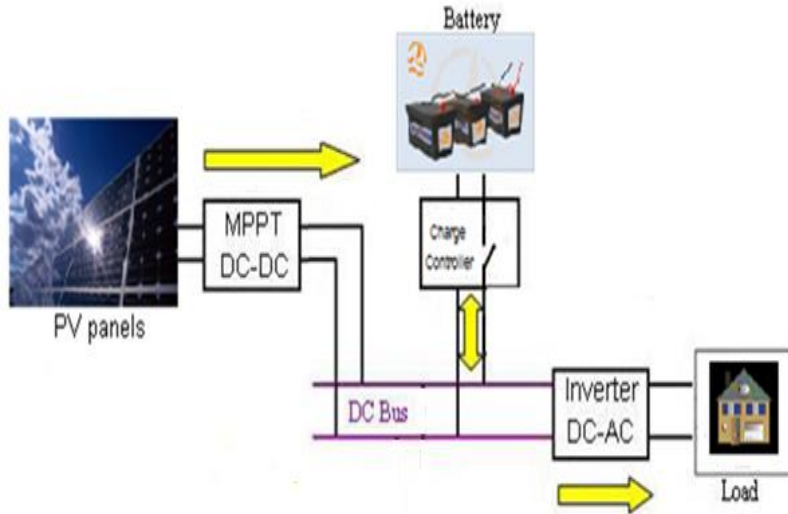
❖ Our research work has relevant contributions such as:

Batteries lifespan is considered at the design phase dynamically during optimization procedure. This approach is new for designing equipment or systems. Replacement time is deduced automatically and integrated to Life Cycle Cost (LCC). Replacement dates are not fixed a priori.

A detailed model that considers inclination of PV panels has been developed and integrated to our Matlab/Simulink dynamic simulator. This model is used to optimize panels' position. Such a tool is not common in literature especially with matlab/Simulink.

Batteries State Of Charge (SOC) limits SOCmin and SOCmax have been considered as optimization decision variables since batteries lifespan highly depends on the Depth Of Discharge (DOD) in order to justify their choice without aggraving the battery.

Standalone photovoltaic system is mostly composed of two power sources: photovoltaic generator and batteries with charge controller.

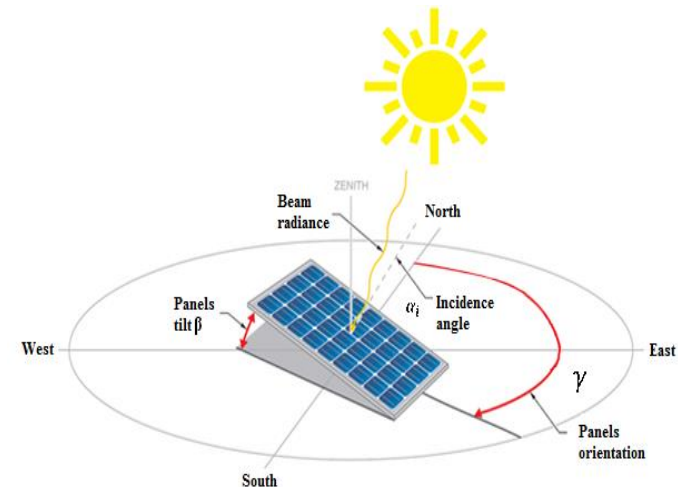


Photovoltaic power

$$P_{pv} = \eta_{pv} \times A_{pv} \times I_r$$

$$I_r = G_b \times R_b + G_d \times \left(\frac{1 + \cos\beta}{2}\right) + G_h \times r \times \left(\frac{1 - \cos\beta}{2}\right)$$

Schematic diagram of a standalone photovoltaic system with storage capabilities



Photovoltaic power

$$P_{pv} = \eta_{pv} \times A_{pv} \times I_r$$

$$I_r = G_b \times R_b + G_d \times \left(\frac{1 + \cos \beta}{2} \right) + G_h \times r \times \left(\frac{1 - \cos \beta}{2} \right)$$

G_b : beam irradiance on a horizontal plane;

R_b : shape factor. It's the ratio between direct irradiance received by panels in comparison with a horizontal plane, expressed by:

$$R_b = \frac{\cos \alpha_i}{\cos \theta}$$

Where α_i and θ are respectively the incidence angle on the panel and the solar zenith angle:

$$\cos \alpha_i = \cos \theta * \cos \beta + \sin \beta * \sin \theta * \cos(\varnothing - \gamma)$$

θ is limited to 89° angle from which irradiance is practically zero after sunset.

β : tilt angle of the collector surface.

γ : panel orientation (degrees): 180° corresponds to South direction.

\varnothing : solar azimuth.

G_d : diffuse irradiance on a horizontal plane.

G_h : global irradiance on a horizontal plane. It corresponds to the irradiance measured by pyrometer.

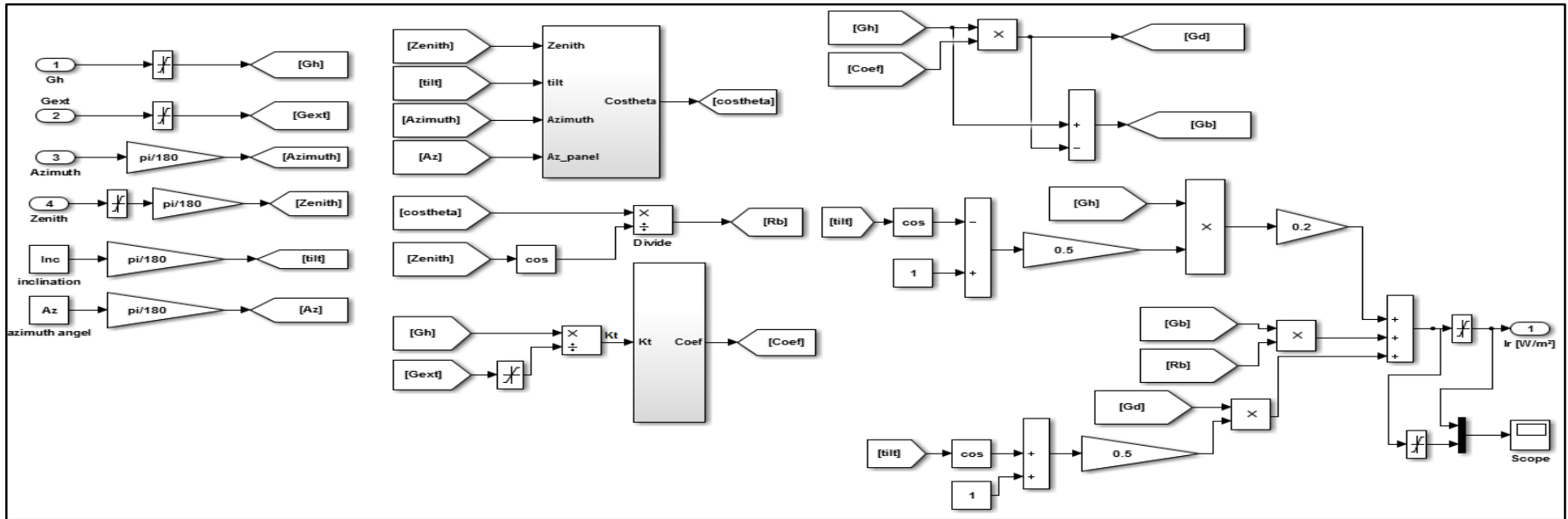
r : represents the diffuse reflectance of the soil (also called ground albedo). It is set to 0.2 if the monthly average temperature is above 0°C .

Photovoltaic power

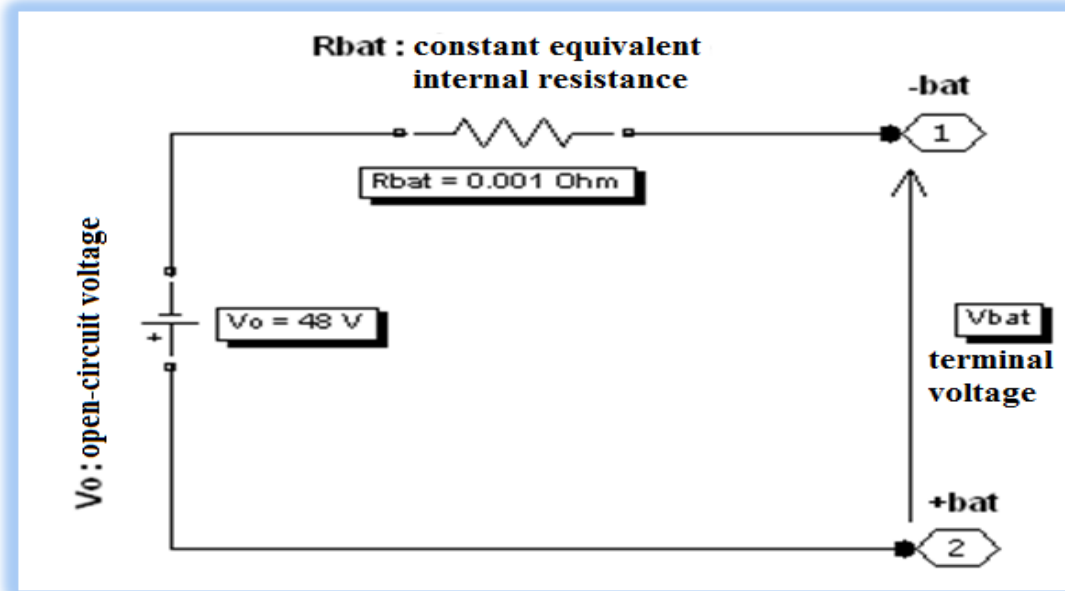
$$P_{pv} = \eta_{pv} \times A_{pv} \times I_r$$

$$I_r = G_b \times R_b + G_d \times \left(\frac{1+\cos\beta}{2}\right) + G_h \times r \times \left(\frac{1-\cos\beta}{2}\right)$$

Thus, using the global horizontal irradiances: measured G_h and extraterrestrial G_0 and sun position data, we have developed a Matlab/Simulink module to calculate the various components of the irradiance I_r incident on tilted panels with any inclination and any orientation. This module is added as a new subsystem to our hybrid power simulator previously developed. With this module, optimization of panels' inclination and orientation is considered for better reliability system, underlining the focus of this paper.



Battery storage model



Ideal Lead-acid battery model

Battery aging model

$$SOH(t) = \frac{Cn(t)}{Cn(t_0)}$$

$$Cn(t) = Cn(t - \Delta t) - Cn(t_0) \times \delta_x \times (SOC(t - \Delta t) - SOC(t))$$

With δ_x the capacity loss coefficient depending on battery technology and Δt the simulation time step. We consider $\delta_{P1omb-tu} = -0,05\%/EFC$ for tubular lead-acid batteries.

Objectives: design and evaluation criteria

Decision variables	Objective /Constraint functions	Feasibility constraints	lower and upper decision variables bounds
<ul style="list-style-type: none"> • A_{pv} : photovoltaic array area • γ : panels 'orientation • β : panels' tilt angle • C_n : batteries nominal capacity • SOC_{min} : batteries SOC lower limit • SOC_{max} : batteries SOC upper limit. 	<ul style="list-style-type: none"> • system Life Cycle Cost (LCC) • Loss of Power Supply Probability (LPSP) 	<ul style="list-style-type: none"> • $A_{pv_min} \leq A_{pv} \leq A_{pv_max}$ • $\gamma_{min} \leq \gamma \leq \gamma_{max}$ • $\beta_{min} \leq \beta \leq \beta_{max}$ • $SOC_{min_l} \leq SOC_{min} \leq SOC_{min_h}$ • $SOC_{max_l} \leq SOC_{max} \leq SOC_{max_h}$ • $C_{n_min} \leq C_n \leq C_{n_max}$ 	<ul style="list-style-type: none"> • $A_{pv_min} = 8 m^2$ • $A_{pv_max} = 15m^2$ • $\gamma_{min} = 150^\circ$ • $\gamma_{max} = 250^\circ$ • $\beta_{min} = 15^\circ$ • $\beta_{max} = 60^\circ$ • $C_{n_{min}} = 150Ah$ • $C_{n_{max}} = 300Ah$ • $SOC_{min_l} = 20 \%$ • $SOC_{min_h} = 40\%$ • $SOC_{max_l} = 75\%$ • $SOC_{max_h} = 100\%$

Objectives: design and evaluation criteria

Decision variables	Objective /Constraint functions	Feasibility constraints	lower and upper decision variables bounds
<ul style="list-style-type: none"> • Apv : photovoltaic array area • γ : panels 'orientation • β : panels' tilt angle • Cn : batteries nominal capacity • $SOCmin$: batteries SOC lower limit • $SOCmax$: batteries SOC upper limit. 	<ul style="list-style-type: none"> • system Life Cycle Cost (LCC) • Loss of Power Supply Probability (LPSP) 	<ul style="list-style-type: none"> • $Apv_{min} \leq Apv \leq Apv_{max}$ • $\gamma_{min} \leq \gamma \leq \gamma_{max}$ • $\beta_{min} \leq \beta \leq \beta_{max}$ • $SOCmin_l \leq SOCmin \leq SOCmin_h$ • $SOCmax_l \leq SOCmax \leq SOCmax_h$ • $Cn_{min} \leq Cn \leq Cn_{max}$ 	<ul style="list-style-type: none"> • $Apv_{min} = 8 m^2$ • $Apv_{max} = 15m^2$ • $\gamma_{min} = 150^\circ$ • $\gamma_{max} = 250^\circ$ • $\beta_{min} = 15^\circ$ • $\beta_{max} = 60^\circ$ • $Cn_{min} = 150Ah$ • $Cn_{max} = 300Ah$ • $SOCmin_l = 20 \%$ • $SOCmin_h = 40\%$ • $SOCmax_l = 75\%$ • $SOCmax_h = 100\%$

1) Cost considerations: minimizing Life Cycle Cost (LCC) of the system

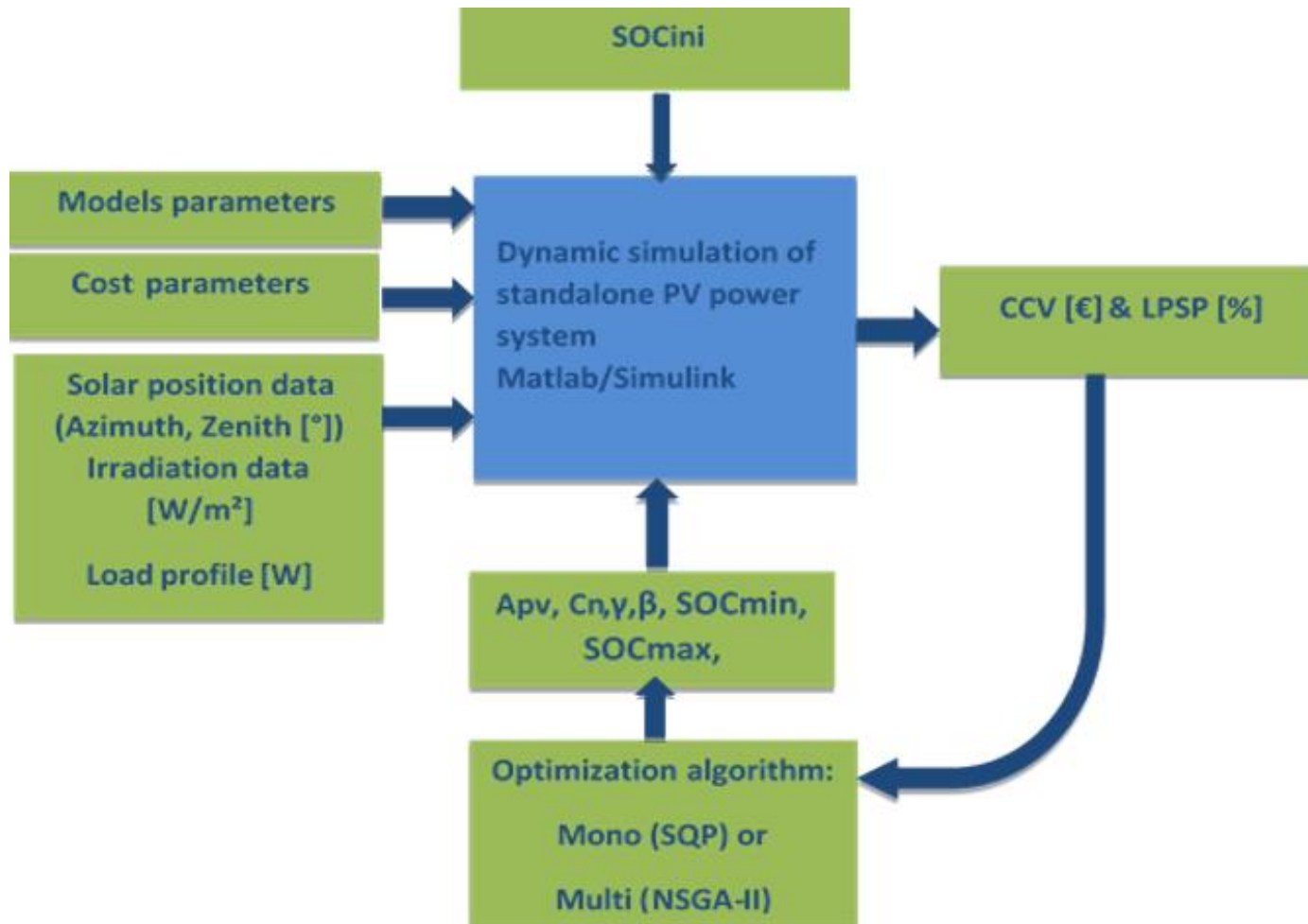
$$LCC[€] = PV_{LCC}[€] + Bat_{LCC}[€] = (650 \times Apv) + 4 \times \left(3 \times \left(1 + \sum_{i=1}^{Nbre\ of\ replacements} 0.95^{replacement_year} \right) \right) \times Cn$$

2) Reliability requirements: minimizing Loss of Power Supply Probability (LPSP)

$$LPSP[\%] : Pr\{Ppv \leq Pdemand\ et\ SOC(t) \leq SOCmin\}$$

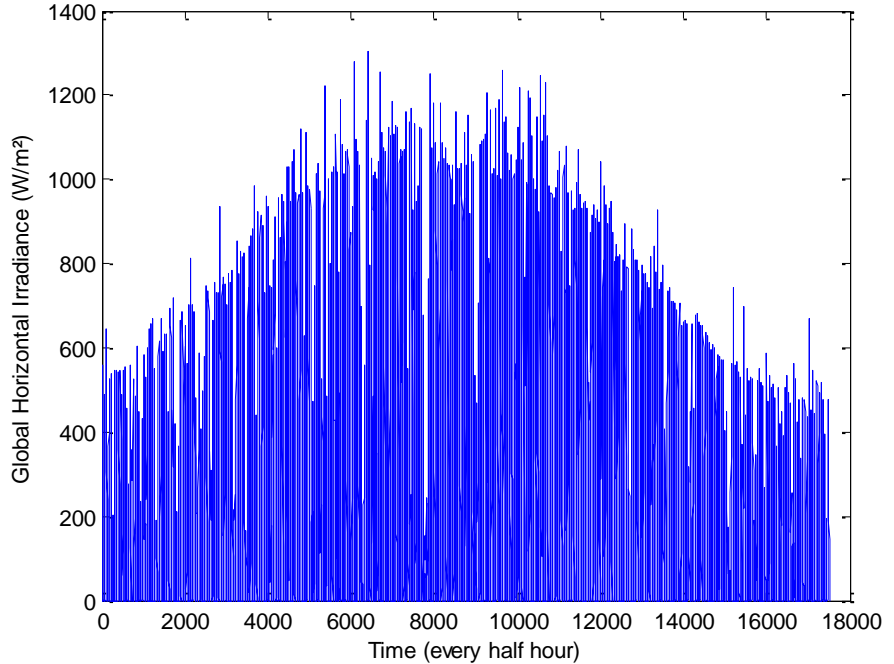
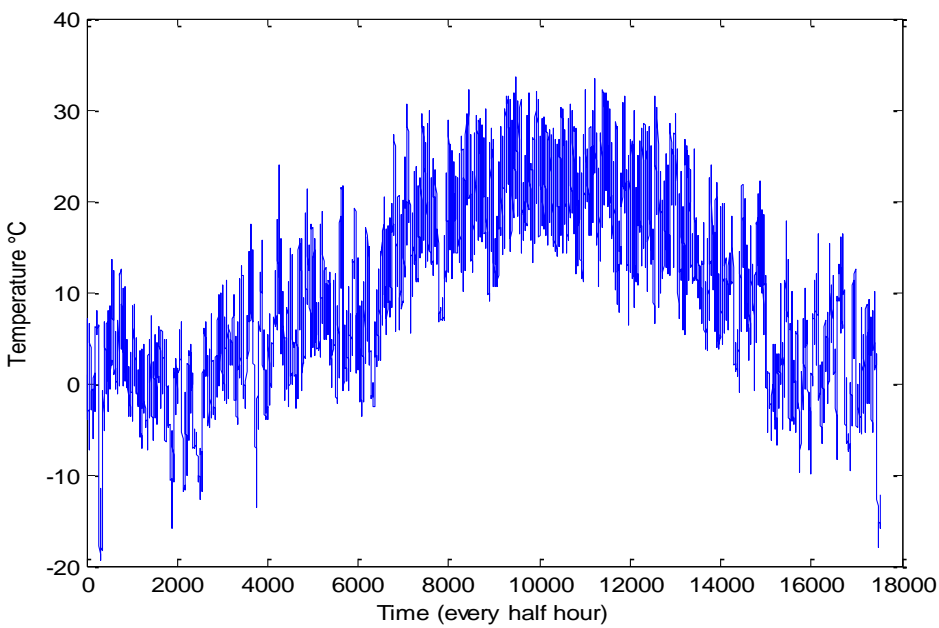
$$LPSP(\Delta t, Apv, \beta, \gamma, Cn, SOCmin, SOCmax) = \frac{\sum_{t=1}^T DE(t, Apv, \beta, \gamma, Cn, SOCmin) \times \Delta t}{\sum_{t=1}^T Pload(t) \times \Delta t}$$

Computational method and algorithm



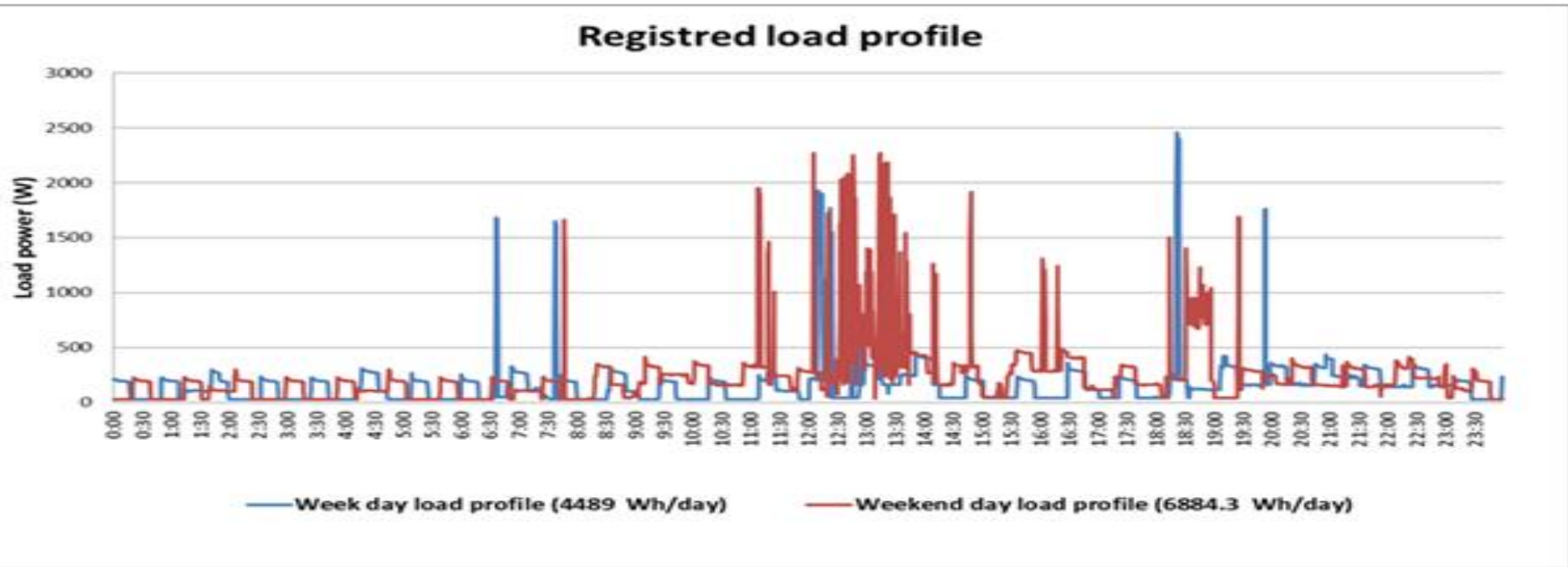
Case study

Half hourly solar radiance and temperature were acquired from the National Wind Technology Centre- Colorado (Latitude: 39° North, Longitude: 105° West, Elevation: 1855 meters) web site for the year 2010 with a low photovoltaic potential [**1857,5 KWh/year/m² Mean : 189 W/m²**]



Case study

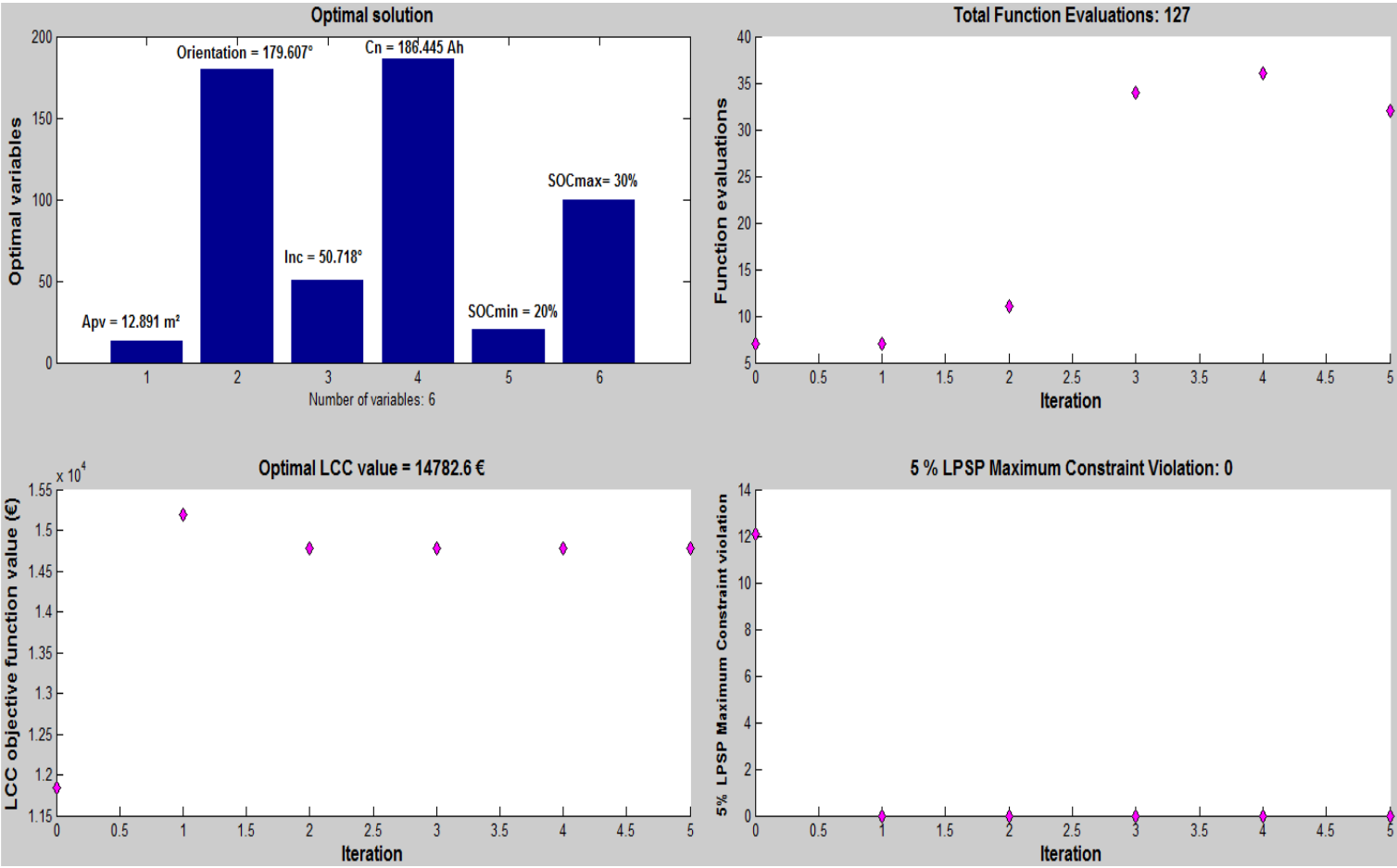
Half-hourly load profile



These profiles were extrapolated for the full year 2010 considering seasonal variations of the electric charge/load and applying correction factors. Thereby, annual electricity consumption of the residence is estimated at **2178 kWh/year in 2010 [Min: 27.6 KW; Max: 3796.3 KW; Mean: 250.5 KW]**.

Case study

SQP non-linear programming optimization results



Case study

SQP non-linear programming optimization results

The design configuration of the PV system that satisfies maximum 5 % LPSP criterion with a small cost is obtained for:

- Photovoltaic modules' installed area $A_{pv} = 13 \text{ m}^2$, eight CHSM 6610P-235 235W panels for instance can be installed.
- Panels' inclination $\beta=51^\circ$ and orientation $\gamma=180^\circ$, nearly.
- Battery bank storage capacity gives $C_n = 186.5 \text{ Ah}$. Four Deep Cycle OutBack Power EnergyCell RE200 12V 200Ah Batteries can be installed in series.
- Battery management bounders: $\text{SOC}_{\min}=20 \%$ and $\text{SOC}_{\max}=100\%$. Now, a justified choice.

With this solution, we expect a cost of about 14782.6 € and a batteries' lifespan of nearly 5.3 years (DR per year = 5.633%), means four batteries replacements in 25 years.

Optimization procedure favorites deep batteries cycling (DOD=80%) in order to reduce batteries cost especially that a variation of 20% on DOD implies a little variation of DR when system is well designed.

This methodology will help designers or installers, advanced users in general. In short or medium term, a tool aid decision could be developed for basic users in order to simplify the process of selection between different criteria.

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