

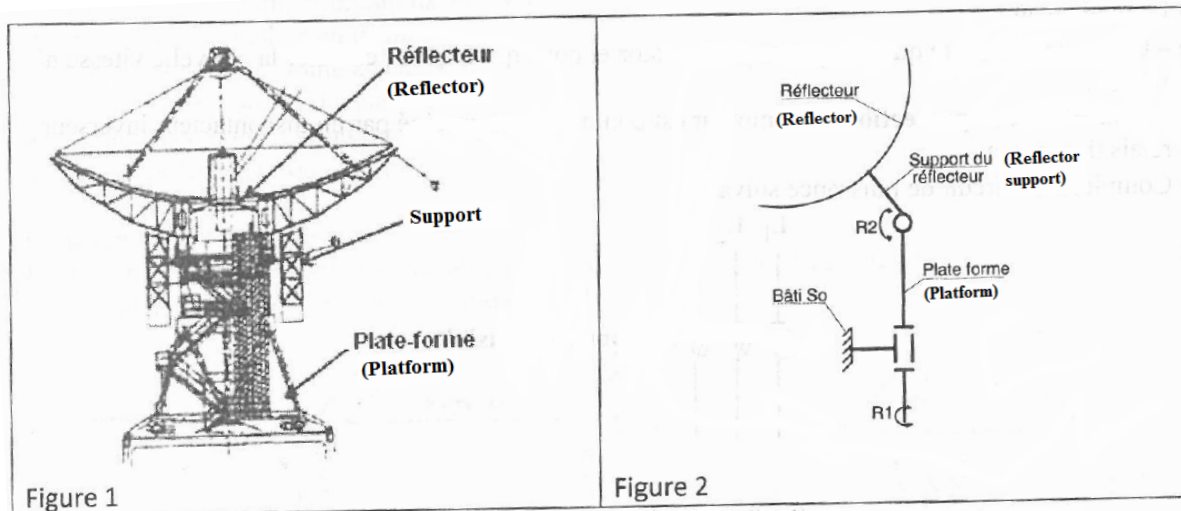
**Exercise: Study of an induction motor in a radio telescope**

Figure 1 shows the overall infrastructure of a radio telescope which may be considered as a measuring instrument. Figure 2 shows its simplified kinematic diagram.

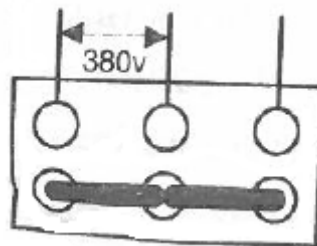
The rotational movement of the platform (R1) with respect to a fixed frame (Bâti S0) is provided by an asynchronous motor (M1) controlled in both directions of rotation. Two tests were performed on this motor:

- **No-load test (“à vide”)** :  $U=380\text{ V}$  between phases, **50 Hz**,  $I_0 = 3\text{ A}$  ,  $P_0 = 500\text{ W}$
- **Rated load test (“à charge nominale”)**:  $U=380\text{ V}$  between phases, **50Hz**,  $I = 10\text{ A}$ ,  $P_a = 5\text{ Kw}$  ,  $n=720\text{ rpm}$  (tr/min).

The resistance of a stator winding is  $R = 0.5\ \Omega$ .



1- The following coupling is performed on the terminal plate :



What type of coupling is? Give the voltages indicated on motor descriptive plate (“sur la plaque signalétique”).

2- Determine the stator iron losses  $P_{fs}$  and mechanical losses  $P_{mec}$  knowing that :

$$P_{fs} = \frac{2}{3} P_{mec}$$

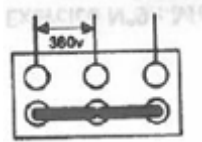
3- Calculate the power factor  $\cos \varphi_0$  at no-load and deduce the reactive power at no-load.

- 4- For operation **at rated load**, calculate :
- a) Stator joule losses  $P_{js}$ .
  - b) Transmitted power  $P_{tr}$ .
  - c) Slip  $g$ .
  - d) Rotor joule losses  $P_{jr}$ .
  - e) Useful output power  $P_u$ .
  - f) Efficiency  $\eta$ .
  - g) Power factor  $\cos \varphi$ .
  - h) Impedance of each stator winding  $Z$ .
- 5- When the load torque applied to M1 is  $T_r = 40 \text{ Nm}$ , is it (motor) capable of radio telescope rotational movement? Justify your answer.

## Correction

*Exercise: Study of an induction motor in a radio telescope*

1) Is performed on the terminal plate the following coupling



The voltages indicated on the descriptive plate: 220v/380v.

2) The stator iron losses  $P_{fs}$  and mechanical losses  $P_{mec}$  with  $P_{fs} = \frac{2}{3} P_{mec}$  :

$$P_0 = P_{fs} + P_{mec} + P_{js_0} = P_{fs} + \frac{3}{2} P_{fs} + 3RI_0^2$$
$$\Rightarrow \frac{5}{2} P_{fs} = P_0 - 3RI_0^2 = 500 - 3 \times 0,5 \times 3^2 = 486,5 \text{ W}$$

Giving:  $P_{fs} = \frac{2 \times 486,5}{5} = 194,6 \text{ W}$  and  $P_{mec} = \frac{3}{2} P_{fs} = \frac{3}{2} \times 194,6 = 292 \text{ W}$

3) Power factor  $\cos \varphi_0$  and reactive power at no-load.

$$\cos \varphi_0 = \frac{P_0}{\sqrt{3} \times U \times I_0} = \frac{500}{\sqrt{3} \times 380 \times 3} = 0,256$$
$$\Rightarrow \varphi_0 = 75^\circ,33 \text{ and } \sin \varphi_0 = 0,967$$

$$Q_0 = \sqrt{3} \times U \times I_0 \times \sin \varphi_0 = \sqrt{3} \times 380 \times 3 \times 0,967 = 1910 \text{ VAR}$$

4) operation at rated load

a) Stator joule losses  $P_{js}$ .

$$P_{js} = 3 \times R \times I^2 = 3 \times 0,5 \times 10^2 = 150 \text{ w}$$

b) Transmitted power  $P_{tr}$ .

$$P_{tr} = P_a - P_{fs} - P_{js} = 5000 - 194,5 - 150 = 4655,5 \text{ W}$$

c) Slip  $g$ .

$$g = \frac{n_s - n}{n_s} = \frac{750 - 720}{750} = 0,04 \text{ so } g\% = 4\%$$

d) Rotor joule losses  $P_{jr}$ .

$$P_{jr} = gP_{tr} = 0,04 \times 4655,5 = 186,22 \text{ W}$$

e) Useful output power  $P_u$ .

$$P_u = P_{tr} - P_{jr} - P_{mec} = 4655,5 - 186,22 - 292 = 4177 \text{ W}$$

f) Efficiency  $\eta$

$$\eta = \frac{P_u}{P_a} = \frac{4177}{5000} = 0,835 \text{ so } \eta\% = 83,5\%$$

g) *Power factor  $\cos \varphi$ .*

$$\cos \varphi = \frac{P_a}{\sqrt{3} \times 380 \times 10} = \frac{5000}{\sqrt{3} \times 380 \times 10} = 0,76$$

h) *Impedance of each stator winding  $Z$ .*

$$Z = \frac{U}{\sqrt{3} \times I} = \frac{380}{\sqrt{3} \times 10} = 22 \Omega$$

5) *Useful Torque :  $T_u = \frac{P_u}{2\pi n} \times 60 = \frac{4177}{2\pi \times 720} \times 60 = 55,43 \text{Nm} > T_r = 40 \text{Nm}$   
So motor M1 is capable of radio telescope rotational movement.*